

# CO<sub>2</sub> utilization as an oxidant in the dehydrogenation of ethylbenzene to styrene over MnO<sub>2</sub>-ZrO<sub>2</sub> catalysts

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## Abstract

MnO<sub>2</sub>-ZrO<sub>2</sub> binary oxide catalytic system was applied for the effective utilization of CO<sub>2</sub> as an oxidant in the ethylbenzene dehydrogenation (EBD) to styrene monomer (SM). MnO<sub>2</sub>-ZrO<sub>2</sub> oxides were prepared by co-precipitation method and characterized as solid solution mixture having surface area more than 100<sup>2</sup> g<sup>-1</sup>. 10% MnO<sub>2</sub>-ZrO<sub>2</sub> mixed oxide catalyst exhibited conversion of 73% with the selectivity of 98% at 650 °C. The MnO<sub>2</sub>-ZrO<sub>2</sub> binary oxides were X-ray amorphous whereas the individual oxides (MnO<sub>2</sub> and ZrO<sub>2</sub>) having much lower surface areas were crystalline in nature. As a result, MnO<sub>2</sub>-ZrO<sub>2</sub> binary oxides exhibited greatly elevated catalytic activity for the conversion of ethylbenzene (EB) than those of individual oxides in the presence of CO<sub>2</sub>. However, in the absence of CO<sub>2</sub> poor catalytic activity and stabilities were observed. Gradual enhancement of activities were demonstrated in the higher CO<sub>2</sub> to EB ratios. Hence, CO<sub>2</sub> had a profound role as a soft oxidant by improving both activity and stability in the EBD over MnO<sub>2</sub>-ZrO<sub>2</sub> mixed oxide catalysts.

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## 1. Introduction

Ethylbenzene dehydrogenation (EBD) is a representative process for the production of styrene (SM), an important monomer for synthetic polymers. This is one of the ten most important industrial petrochemical processes. However, the present industrial process is thermodynamically limited, energy consuming, super heated steam obligatory, coke-deactivating, partially active, and poorly selective [1]. Alternatively, oxidative EBD has been proposed in order to circumvent some of the cited difficulties [2]. However, in the oxidative dehydrogenation process the usage of O<sub>2</sub> (strong oxidant) produces unwanted by-products (oxygenates) along with SM resulting in low selectivity of SM [3]. Hence, alternative oxidative EBD with CO<sub>2</sub> oxidant has been emerging as a potential process [4–6], because CO<sub>2</sub> utilization offer several advantages in catalysis such as acceleration of the reaction rate, enhancement in product selectivity, alleviation of thermodynamic equilibrium limitations, suppression of total oxidation, prolonging of catalyst life, and prevention of hot spots on

the catalyst surface. Based on these unique characteristics it has been coined as a soft oxidant [7,8].

Since the present commercial iron based catalysts are ineffective for the EBD in the presence of CO<sub>2</sub>, intensive explorations have emerged recently in order to develop compatible catalytic systems that can operate effectively with CO<sub>2</sub>. Mimura et al. [9–11] and Badstube et al. [12,13] have investigated Al<sub>2</sub>O<sub>3</sub> and active carbon (AC) supported alkali metal promoted iron oxide based catalysts, respectively, for EBD in the presence of CO<sub>2</sub>. The effective utilization of CO<sub>2</sub> was accomplished in our earlier publications over zeolite and ZrO<sub>2</sub> supported iron oxides [8,14], Al<sub>2</sub>O<sub>3</sub> supported vanadium and vanadium-antimony oxide catalysts [15–17]. In our recent report, the influence of CO<sub>2</sub> over ZrO<sub>2</sub> has been described, wherein enhancement in conversion of EB as well as selectivity towards SM in presence of CO<sub>2</sub> oxidant was observed [18]. Furthermore, catalytic activity of ZrO<sub>2</sub> has been significantly improved when it was mixed with TiO<sub>2</sub> [19]. Presently, the study has been extended to MnO<sub>2</sub>-ZrO<sub>2</sub> mixed oxides, based on our results on TiO<sub>2</sub>-ZrO<sub>2</sub> mixed oxide catalysts. In the present publication, apart from the general catalytic activity studies of MnO<sub>2</sub>-ZrO<sub>2</sub> mixed oxides in the dehydrogenation of EB to SM, the role of CO<sub>2</sub> as a soft oxidant has been delineated.

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## 2. Experimental

### 2.1. Catalyst preparation

MnO<sub>2</sub>-ZrO<sub>2</sub> mixed oxides were prepared by co-precipitation method taking zirconyl nitrate and manganese nitrate as precursors and aqueous ammonia solution was used as a hydrolyzing agent. In a typical experiment, 0.1 M mixed aqueous solution of respective precursors was stirred at room temperature for 0.5 h. After attainment of homogeneous solution, requisite amount of aqueous ammonia solution was added until the pH of the solution reached 9 and the stirring was continued further 1 h followed by aging at 100 °C for 12 h. The resultant precipitate was filtered off under reduced pressure and washed thoroughly with water and dried at 120 °C for 12 h in oven and finally calcined at 550 °C for 6 h in a muffle furnace. Individual oxides (MnO<sub>2</sub> and ZrO<sub>2</sub>) were prepared adopting the same procedure. In order to find out the EBD activity on MnO<sub>2</sub> and ZrO<sub>2</sub> solid solution, 50% MnO<sub>2</sub>-ZrO<sub>2</sub> mixed oxide was further calcined at 650, 750 and 850 °C.

### 2.2. Catalyst characterization

BET surface area of the catalyst was measured by nitrogen adsorption at liquid nitrogen temperature (−196 °C) using pulse chemisorb 2705 (Micromeritics Instrument Co., USA). The catalysts were evacuated for 2 h at 200 °C prior to the experiment. Bulk density was estimated on the basis of mass and volume of the catalysts.

X-ray powder diffraction patterns were recorded on a Rigaku X-ray Diffractometer (Multiflex, Japan), with Ni filtered Cu K $\alpha$  radiation ( $\lambda = 1.5406 \text{ \AA}$ ) operated at 50 kV and 50 mA in the  $2\theta$  range of 10–90° with scan speed of  $4^\circ \text{ min}^{-1}$ .

Temperature programmed desorption (TPD) of NH<sub>3</sub> (5% NH<sub>3</sub> in helium) and CO<sub>2</sub> (5% CO<sub>2</sub> in helium) studies were performed using pulse chemisorb 2705 (Micromeritics Instrument Co., USA). In the individual TPD experiments either NH<sub>3</sub> or CO<sub>2</sub> was adsorbed at 100 °C for 30 min and purged at the same temperature with helium gas (20 ml/min) for the removal of the physisorbed gasses, followed by desorption of the gasses from 100 to 700 °C at a heating rate of 5 °C/min.

### 2.3. Reaction and analysis

The catalytic activity studies were performed in a fixed bed continuous flow stainless steel reactor (i.d., 4.5 mm and length, 300 mm). Typically, 1.0 g of catalyst sample was loaded into the reactor with the support of quartz wool. The reactor was heated to 600 °C in presence of N<sub>2</sub> flow (20 ml/min) at the rate of 2 °C/min and pretreated at this temperature for 2 h then altered to the reaction temperature and pretreated with CO<sub>2</sub> (20 ml/min) prior to conducting the reaction for 0.5 h. EB was introduced by a peristaltic pump with a feed flow rate of 9.8 mmol/h along with either N<sub>2</sub> or N<sub>2</sub> + CO<sub>2</sub>. Unless otherwise specified contact time (W/F) is 16.73 g h/mole at 5.1 molar ratio of CO<sub>2</sub> to EB. Contact time (W/F) is defined as the weight

Table 1

BET surface areas and bulk densities of MnO<sub>2</sub>-ZrO<sub>2</sub> mixed oxide catalysts

Catalyst	Surface area (m <sup>2</sup> /g)	Bulk density (g/cm <sup>3</sup> )
ZrO <sub>2</sub>	25	1.71
MnO <sub>2</sub>	5	1.63
5% MnO <sub>2</sub> -ZrO <sub>2</sub>	72	1.49
10% MnO <sub>2</sub> -ZrO <sub>2</sub>	106	1.28
20% MnO <sub>2</sub> -ZrO <sub>2</sub>	108	1.21
25% MnO <sub>2</sub> -ZrO <sub>2</sub>	101	1.16
50% MnO <sub>2</sub> -ZrO <sub>2</sub>	106	0.99

of the catalyst in grams divided by the sum of the flow rates of the reactants and nitrogen in moles per hour. Gaseous and liquid products were analyzed simultaneously by on-line GC (Younlin Instrument, Acme 6000 series, Korea) equipped with TCD and FID. Poropak N 80/100 column (6 ft  $\times$  1/8") was used for the analysis of gaseous products such as hydrogen, nitrogen, carbon monoxide, methane, and carbon dioxide. HP-innowax column (30 m long, 0.32 mm i.d. and 0.25  $\mu\text{m}$  film thickness) was used for the analysis of liquid products in which, SM is the major product, and benzene, toluene, benzaldehyde, and acetophenone were minor/trace products.

## 3. Results and discussion

### 3.1. Physico-chemical properties of MnO<sub>2</sub>-ZrO<sub>2</sub> mixed oxides

The surface areas of individual oxides of MnO<sub>2</sub>, ZrO<sub>2</sub> and their mixed oxides (MnO<sub>2</sub>-ZrO<sub>2</sub>) were depicted in Table 1. The surface areas of all the mixed oxides are much higher than that of individual oxides, whereas the bulk densities are lighter than either MnO<sub>2</sub> or ZrO<sub>2</sub> (Table 1). The mixed oxides were X-ray amorphous or poorly crystalline, whereas both MnO<sub>2</sub> and ZrO<sub>2</sub> are purely crystalline (Fig. 1). The TPD of NH<sub>3</sub> and CO<sub>2</sub> of individual oxides (MnO<sub>2</sub> and ZrO<sub>2</sub>) and 10% MnO<sub>2</sub>-ZrO<sub>2</sub> mixed oxide reveal that the individual oxides possessed fewer number of acidic as well as basic sites than 10% MnO<sub>2</sub>-ZrO<sub>2</sub> mixed oxide (Figs. 2 and 3). The mixed oxides calcined at higher temperatures (>650 °C) were transformed into crystalline materials (Fig. 4). The formation of amorphous, high

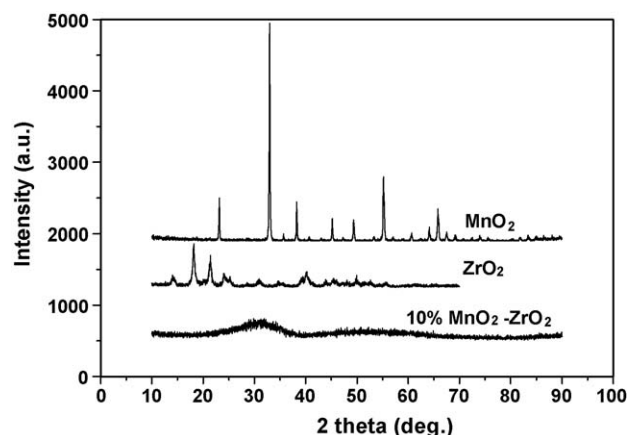


Fig. 1. XRD patterns of MnO<sub>2</sub>, ZrO<sub>2</sub> and 10% MnO<sub>2</sub>-ZrO<sub>2</sub> calcined at 550 °C.

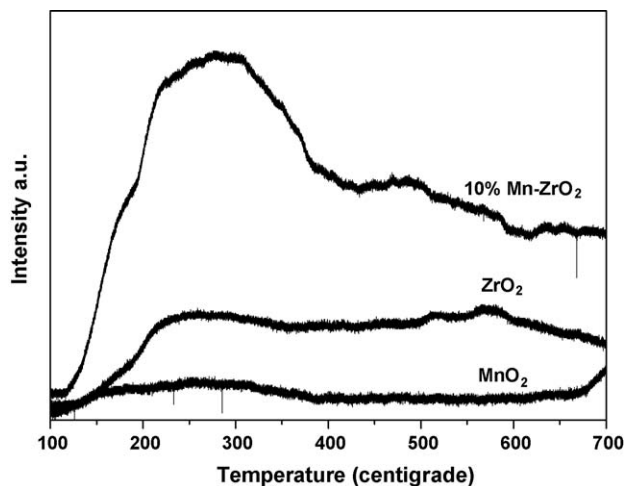


Fig. 2.  $\text{NH}_3$  TPD patterns of  $\text{MnO}_2$ ,  $\text{ZrO}_2$  and 10%  $\text{MnO}_2$ - $\text{ZrO}_2$ .

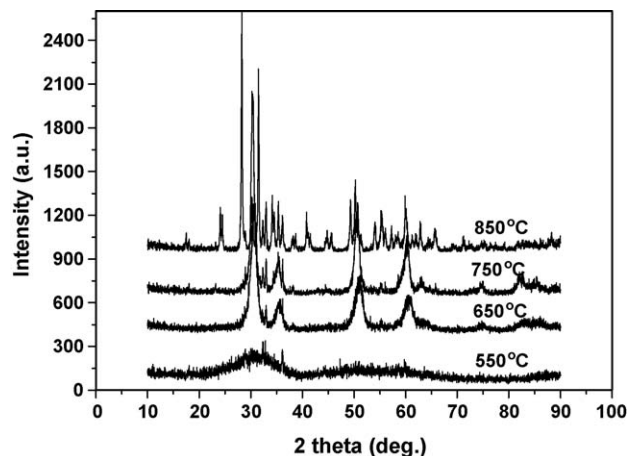


Fig. 4. XRD patterns of 50%  $\text{MnO}_2$ - $\text{ZrO}_2$  calcined at different temperatures.

surface area, and low density mixed oxide of  $\text{ZrO}_2$  based binary oxides during the stages of preparation are reported [19,20]. In accordance with our previous publication,  $\text{ZrO}_2$  contributes towards the activation of  $\text{CO}_2$  based on its crystallographic phases [18] and acid–base capacities [20]. The addition of  $\text{MnO}_2$ , chosen not only for the enhancement in acid base properties of mixed oxide but also for its redox properties [21], anticipated the improved performance for the dehydrogenation of EB to SM in presence of  $\text{CO}_2$ .

### 3.2. Catalytic activity

EBD over  $\text{MnO}_2$ ,  $\text{ZrO}_2$ , and 10%  $\text{MnO}_2$ - $\text{ZrO}_2$  mixed oxide in the presence of  $\text{CO}_2$  was shown in the Fig. 5. The superior activity of  $\text{MnO}_2$ - $\text{ZrO}_2$  mixed oxide over its respective individual oxides might be due to generation of active sites during the stages of mixed oxide catalyst preparation as described above. Mimura and Saito also reported that either  $\text{Al}_2\text{O}_3$  or  $\text{Fe}_2\text{O}_3$  is inferior to  $\text{Fe}_2\text{O}_3/\text{Al}_2\text{O}_3$  catalysts for the EBD in the presence of  $\text{CO}_2$  and explained that special interaction between iron oxide and alumina might be necessary for higher

activity [9]. EB conversion on  $\text{MnO}_2$  was higher than  $\text{ZrO}_2$  but the average selectivity (total 6 h selectivity averaged) was lower. The combination of redox and acid base bi-functional mechanism might be responsible for the higher activity of  $\text{MnO}_2$ - $\text{ZrO}_2$  mixed oxides. However, further studies are necessary for the elucidation of the mechanism. Marginal decrease in activity of  $\text{MnO}_2$ ,  $\text{ZrO}_2$ , and  $\text{MnO}_2$ - $\text{ZrO}_2$  mixed oxide might be due to coke deposition.

The influence of  $\text{MnO}_2$  and  $\text{ZrO}_2$  composition in the EBD with time on stream in the presence of  $\text{CO}_2$  was shown in Fig. 6. Almost all the studied compositions were catalytically active with little variation. However, 10%  $\text{MnO}_2$ - $\text{ZrO}_2$  mixed oxide catalyst was found to be the best. It showed that the contribution of the  $\text{ZrO}_2$  surface was clearly necessary for the effective activation of  $\text{CO}_2$ .

In order to find out the role of pretreatment, the catalyst was treated with  $\text{CO}_2$  (20 ml/min) at the reaction temperature at different lengths of time from 0.5 to 12 h (Fig. 7). The catalysts

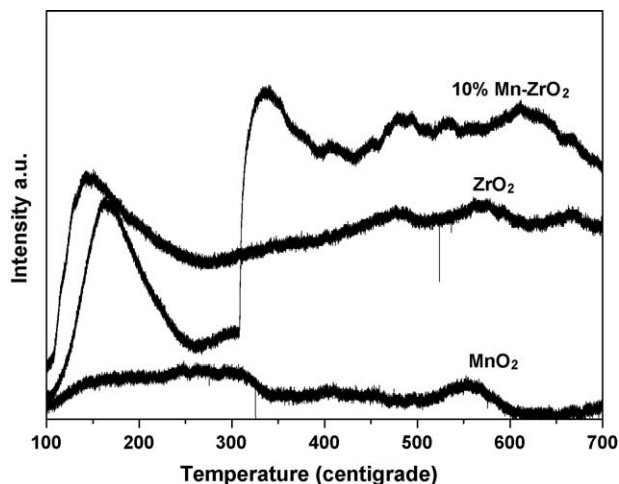


Fig. 3.  $\text{CO}_2$  TPD patterns of  $\text{MnO}_2$ ,  $\text{ZrO}_2$  and 10%  $\text{MnO}_2$ - $\text{ZrO}_2$ .

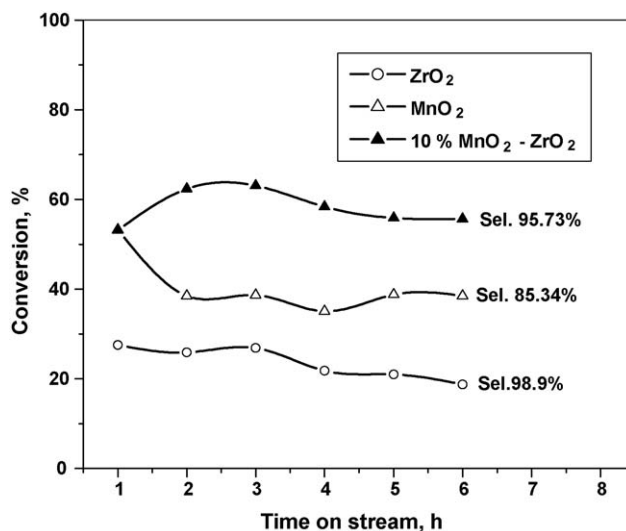


Fig. 5. EBD activity of  $\text{MnO}_2$ ,  $\text{ZrO}_2$ , and 10%  $\text{MnO}_2$ - $\text{ZrO}_2$  mixed oxide catalyst. Reaction conditions: catalyst weight = 1.0 g, temperature = 600 °C,  $\text{CO}_2/\text{EB}$  = 5.1 (molar ratio),  $W/F$  = 16.73  $\text{g}_{\text{cat}}/\text{h}/\text{mole}$ .

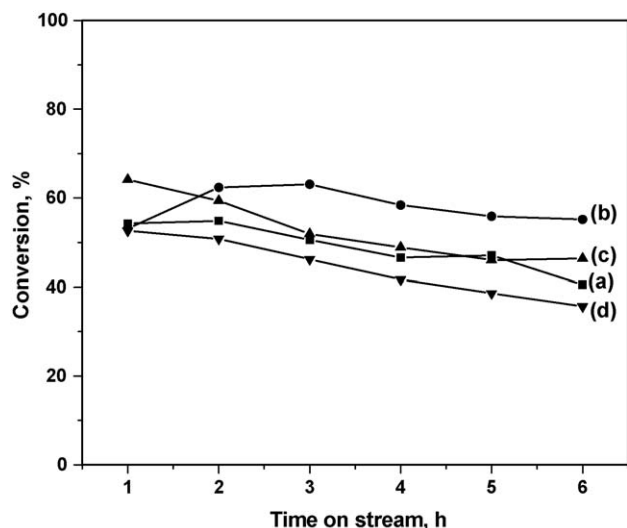


Fig. 6. EBD activity over different loadings MnO<sub>2</sub>-ZrO<sub>2</sub> mixed oxide catalysts (a) 5% MnO<sub>2</sub>-ZrO<sub>2</sub>; (b) 10% MnO<sub>2</sub>-ZrO<sub>2</sub>; (c) 20% MnO<sub>2</sub>-ZrO<sub>2</sub>; (d) 50% MnO<sub>2</sub>-ZrO<sub>2</sub>. Reaction conditions: catalyst weight = 1.0 g, temperature = 600 °C, CO<sub>2</sub>/EB = 5.1 (molar ratio), W/F = 16.73 g<sub>cat</sub> h/mole.

pretreated with CO<sub>2</sub> for 0.5–1 h showed marginal hike in activity. The reason for the small hike in activity with CO<sub>2</sub> pretreatment might be adsorption of certain amount of CO<sub>2</sub> facilitates the reaction instead of competitive adsorption of both EB and CO<sub>2</sub> at a time. The catalysts pretreated for more than 1 h showed reduction in activity, but the total deactivation has not been detected even after 12 h pretreatment with CO<sub>2</sub>. The decrease in activity with longer pretreatment periods might be due to neutralization of some of the active basic sites by CO<sub>2</sub>.

The catalytic activity of 50% MnO<sub>2</sub>-ZrO<sub>2</sub> mixed oxides calcined at different temperatures for the EBD in presence of CO<sub>2</sub> was shown in Fig. 8. The MnO<sub>2</sub>-ZrO<sub>2</sub> mixed oxide calcined at 550 °C exhibited higher conversion and selectivity. The catalytic activity decreased with increased calcination temperatures. The change in phases from amorphous to

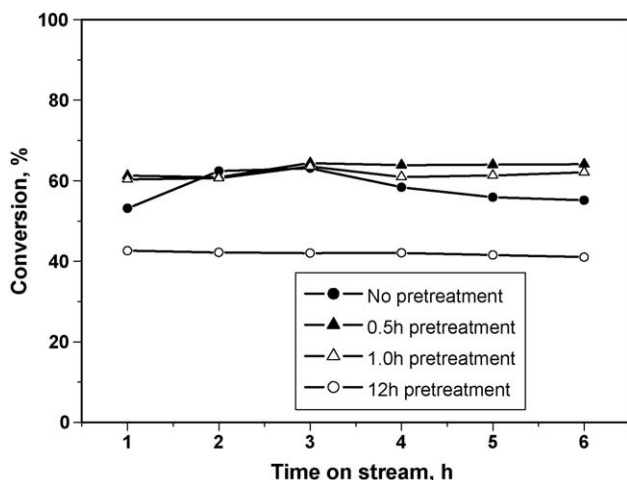


Fig. 7. EBD activity with respect to pretreatment temperature over 10% MnO<sub>2</sub>-ZrO<sub>2</sub> mixed oxide catalyst. Reaction conditions: catalyst weight = 1.0 g, temperature = 600 °C, CO<sub>2</sub>/EB = 5.1 (molar ratio), W/F = 16.73 g h/mole.

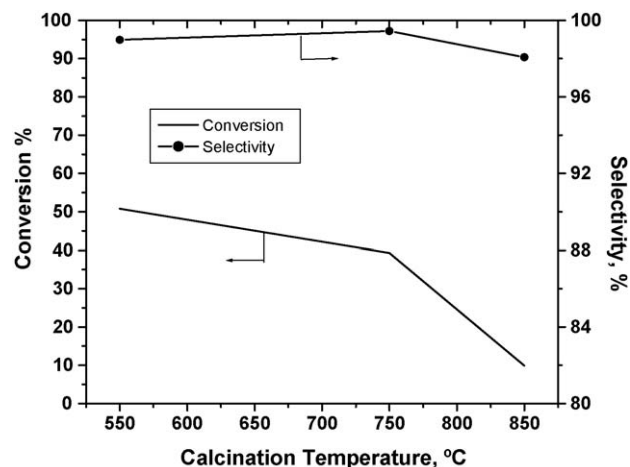


Fig. 8. EBD activity with respect to calcination temperature over 50% MnO<sub>2</sub>-ZrO<sub>2</sub> mixed oxide catalyst. Reaction conditions: catalyst weight = 1.0 g, temperature = 600 °C, CO<sub>2</sub>/EB = 5.1 (molar ratio), W/F = 16.73 g h/mole.

crystalline (Fig. 4) drastically decreased the EB conversion and SM selectivity.

### 3.3. Effects of reaction conditions

EB conversion and SM selectivity as a function of reaction temperature, was shown in Fig. 9. The conversion of EB increased monotonically with increase in reaction temperature from 450 to 650 °C. Surprisingly the selectivity to SM was maintained at 98% at higher temperatures (600 and 650 °C). Sugino et al. reported that the conversion of EB increased sharply with reaction temperature over active carbon supported iron catalyst wherein the yield of SM was 20% at 500 °C and rose to 47% at 600 °C but the selectivity dropped from 99 to 85% [22]. In a recent report [23], decrease in SM selectivity with reaction temperature over Cr-MCM-41 was mainly due to

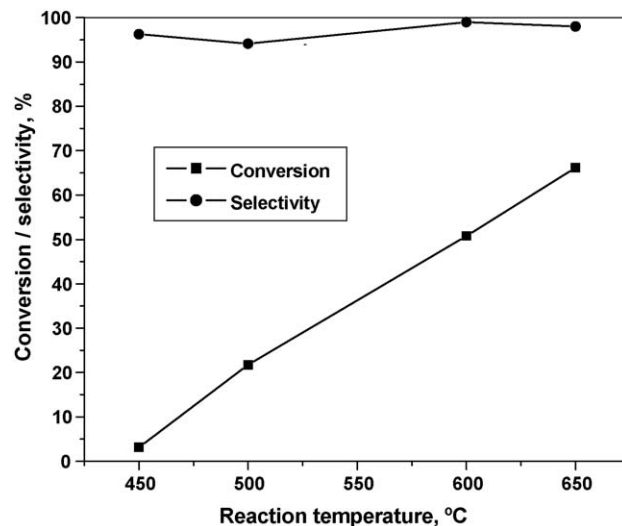


Fig. 9. EBD activity on 50% MnO<sub>2</sub>-ZrO<sub>2</sub> mixed oxide catalyst with respect to reaction temperature. Reaction conditions: catalyst weight = 1.0 g, CO<sub>2</sub>/EB = 5.1 (molar ratio), W/F = 16.73 g h/mole.



Table 2  
EBD activity on 25% MnO<sub>2</sub>-ZrO<sub>2</sub> in the presence and absence of CO<sub>2</sub>

TOS (h)	CO <sub>2</sub>			
	Presence		Absence	
	EB conversion (%)	SM selectivity (%)	EB conversion (%)	SM selectivity (%)
1	30.21	98.68	33.72	95.46
2	45.38	98.29	53.33	99.04
3	53.82	98.85	53.41	98.71
4	51.06	99.12	46.50	99.18
5	48.61	98.79	44.28	99.14
6	46.88	98.96	45.67	99.17
7	44.21	99.38	38.94	98.92
8	43.29	98.81	37.94	98.21
9	40.80	98.08	37.33	98.93
10	39.25	97.88	36.53	98.80

Reaction conditions: temperature = 600 °C, pressure = 1 atm, catalyst weight = 1.0 g, CO<sub>2</sub> or N<sub>2</sub>/EB = 5.1 (molar ratio), W/F = 16.73 g h/mole.

enhancement in benzene and toluene formation. The sharp increase, in EB conversion with reaction temperatures over MnO<sub>2</sub>-ZrO<sub>2</sub> mixed oxides was observed. Similar behavior in EB conversion with reaction temperature was reported in earlier publications [22,23].

The effect of contact time (W/F) on the conversion of EB was shown in Fig. 10. The data were obtained by varying the weight of the catalyst keeping the flow rates of EB as well as CO<sub>2</sub> constant at 10.2 molar ratios of CO<sub>2</sub> to EB. The conversion of EB was 46.81% at the contact time of 8.37 g h/mole. The EB conversion was considerably increased to 72.81% with increase in contact time to 16.73 g h/mole. Further increase of contact time to 25.1 and 33.46 g h/mole, increased EB conversions to 75.33 and 78.15%, respectively. However as this increase in contact time did not influence the EB conversion considerably, the contact time was fixed at 16.73 g h/mole.

The catalytic activity of 25% MnO<sub>2</sub>-ZrO<sub>2</sub> mixed oxide catalyst for EBD in the presence of CO<sub>2</sub> and its absence was

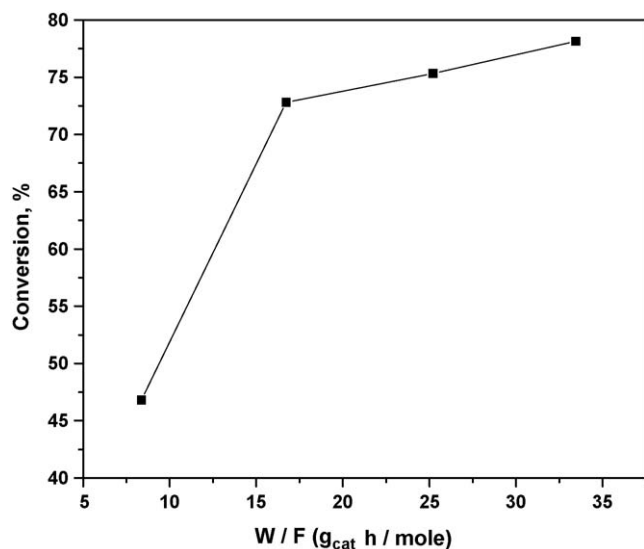


Fig. 10. Variation of EBD activity with contact time over 10% MnO<sub>2</sub>-ZrO<sub>2</sub> mixed oxide. Reaction conditions: catalyst weight = 1.0 g, temperature = 650 °C, CO<sub>2</sub>/EB = 10.2 (molar ratio).

shown in Table 2. The selectivity of SM is always constant at about 98% under either N<sub>2</sub> or CO<sub>2</sub> atmosphere, whereas the conversion under CO<sub>2</sub> atmosphere was higher than under N<sub>2</sub> atmosphere except for the first 2 h of time on stream. The initial low activity was observed with CO<sub>2</sub> when the catalyst was not pretreated with CO<sub>2</sub>. The constant selectivity with decreasing conversion under N<sub>2</sub> atmosphere represents that both the yields of SM as well as by-products were diminished with the time on stream. In other words, the catalyst deactivation rate was more under N<sub>2</sub> atmosphere rather than CO<sub>2</sub> atmosphere. It can be explained that the catalyst deactivation might be taking place due to coke deposition. In the presence of CO<sub>2</sub>, certain amount of coke might be converting into CO [24]. As a result the rate of catalyst deactivation decreases. Similar catalytic behavior in the presence of CO<sub>2</sub> over Cr/Cab-O-Sil catalyst for the EBD was reported [24]. The maximum difference in conversion of EB was 5% over 10% MnO<sub>2</sub>-ZrO<sub>2</sub> mixed oxide catalyst at 600 °C in the presence of CO<sub>2</sub> than that in the absence of CO<sub>2</sub>. The yield of SM in the presence of CO<sub>2</sub> was 2.5 times higher than that in the absence of CO<sub>2</sub> at 550 °C over V/MgO catalyst [25].

The influence of CO<sub>2</sub> was also determined by varying the feed composition of CO<sub>2</sub> and EB. The conversion of EB at different feed ratios of CO<sub>2</sub> to EB over 10% MnO<sub>2</sub>-ZrO<sub>2</sub> mixed oxide catalyst at 650 °C was depicted in Fig. 11. The conversion of EB in the absence of CO<sub>2</sub> was 64.25%, which was increased to 72.82% when N<sub>2</sub> (N<sub>2</sub>/EB = 10.2) was replaced by CO<sub>2</sub> (CO<sub>2</sub>/EB = 10.2) in the feed. The increase in the conversion of EB was observed with increase in the amount of CO<sub>2</sub> in the feed up to CO<sub>2</sub> to EB ratio of 10.2. At a CO<sub>2</sub> to EB ratio of 15.3, the conversion of EB was decreased. Similar trend was observed in the catalytic activity pattern of activated carbon supported iron catalysts for the dehydrogenation of EB [12]. It seems that optimum concentration of surface CO<sub>2</sub> could be required to get high stability and activity due to the competitive adsorption of CO<sub>2</sub> and EB onto the catalyst surface. Therefore, 10% MnO<sub>2</sub>-ZrO<sub>2</sub> mixed oxide catalyst showed the optimum activity and stability at the CO<sub>2</sub> to EB ratio of 10.2 due to the adequate balance for the adsorption and activation of CO<sub>2</sub> and EB.

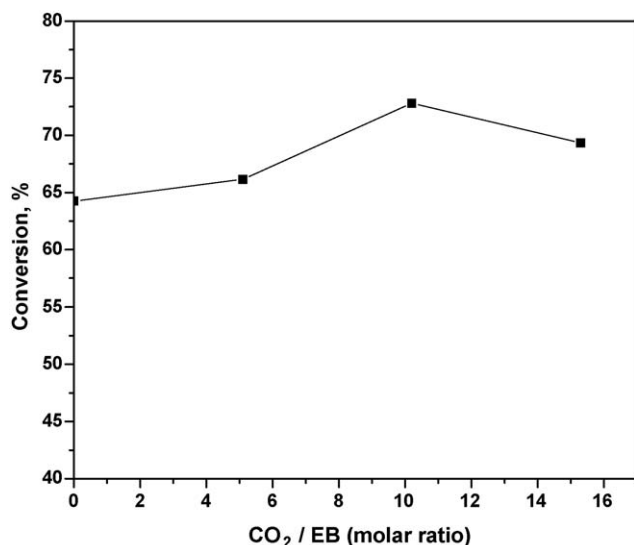


Fig. 11. EB conversions on 10% MnO<sub>2</sub>-ZrO<sub>2</sub> with respect to feed ratio (CO<sub>2</sub>/EB). Reaction conditions: catalyst weight = 1.0 g, temperature = 650 °C, W/F = 16.73 g<sub>cat</sub> h/mole.

#### 4. Conclusions

MnO<sub>2</sub>-ZrO<sub>2</sub> mixed oxide catalysts were demonstrated to be highly active in the dehydrogenation of EB to SM in the presence of CO<sub>2</sub>. The best results were obtained over 10% of MnO<sub>2</sub> loaded on ZrO<sub>2</sub> catalyst at 650 °C with a conversion of 73% and the selectivity to styrene was about 98%. CO<sub>2</sub> attributed to the enhancement in catalytic activity by the oxidative conversion as well as catalytic life by suppressing the coke deposition.

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